EVALUATION OF SOME THERMAL POWER CYCLES FOR USE IN SPACE

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ABSTRACT Production of power in space for terrestrial use is of great interest in view of the rapidly rising power demand and its environmental impacts. Space also offers a very low temperature, making it a perfect heat sink for power plants, thus offering much higher efficiencies. This paper focuses on the evaluation and analysis of thermal Brayton, Ericsson and Rankine power cycles operating at space conditions on several appropriate working fluids. 1. Under the examined conditions, the thermal efficiency of Brayton cycles reaches 63%, Ericsson 74%, and Rankine 85%. These efficiencies are significantly higher than those for the computed or real terrestrial cycles: by up to 45% for the Brayton, and 17% for the Ericsson; remarkably 44% for the Rankine cycle even when compared with the best terrestrial combined cycles. From the considered working fluids, the diatomic gases (N_2 and H_2) produce somewhat better efficiencies than the monatomic ones in the Brayton and Rankine cycles, and somewhat lower efficiencies in the Ericsson cycle. The Rankine cycles require radiator areas that are larger by up to two orders of magnitude than those required for the Brayton and Ericsson cycles. The results of the analysis of the sensitivity of the cycle performance parameters to major parameters such as turbine inlet temperature and pressure ratio are presented, and the effects of the working fluid properties on cycle efficiency and on the power production per unit radiator area were explored to allow decisions on the optimal choice of working fluids.

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Specific entropy [kJ/kg·K]

Keywords: Power cycles, Space power, Space, Brayton cycle, Ericsson cycle, Rankine cycle

Nomenclature

$Area [m^2]$	t	Radiator wall thickness [m]
Evergy [k]/kg]	Т	Temperature [K]
Speed of sound [m/s]	TIT	Turbine inlet temperature [K]
Mass flow rate [kg/s]	U	Overall heat transfer coefficient
Convective heat transfer coefficient		$[W/m^2 \cdot K]$
$[W/m^2,K]$	W	Power output [kW]
Radiative heat transfer coefficient	W	Specific power output [kJ/kg]
$[W/m^2 K]$	Greek	
	δ	Radiator flow gap [m]
Thermal conductivity constant [W/m K]	ΔT_{lm}	Log mean temperature difference [K]
Nusselt number	£	Emittance
Pressure [bar]	e	Exergy efficiency
Prandtl number	10	Thermal efficiency
Heat duty [kW]	η_I	Disease in the second s
Reynolds number	π	Pressure ratio
Total thermal resistance [K/W]	σ_{sb}	Stefan-Boltzmann constant [5.67(10°)
	Area [m ²] Exergy [kJ/kg] Speed of sound [m/s] Mass flow rate [kg/s] Convective heat transfer coefficient [W/m ² ·K] Radiative heat transfer coefficient [W/m ² ·K] Thermal conductivity constant [W/m·K] Nusselt number Pressure [bar] Prandtl number Heat duty [kW] Reynolds number Total thermal resistance [K/W]	Area $[m^2]$ tExergy $[kJ/kg]$ TSpeed of sound $[m/s]$ TITMass flow rate $[kg/s]$ UConvective heat transfer coefficientW $[W/m^2 \cdot K]$ WRadiative heat transfer coefficientW $[W/m^2 \cdot K]$ GreekThermal conductivity constant $[W/m \cdot K]$ δ Nusselt number ΔT_{lm} Pressure $[bar]$ ϵ Prandtl number π Heat duty $[kW]$ η_l Reynolds number π Total thermal resistance $[K/W]$ σ_{sb}

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 $W/kg \cdot K^4$] Ψ Power produced per unit radiator area $[kW/m^2]$

Subscripts

in	Inlet	
out	Outlet	
Η	High	
L	Low	
rad	Radiator	
	Space	

- s Space t Total
- 1..10 States on the cycle flow sheet